

بسمه تعالى



نگرش نوین بر طراحی و اجرای پی های عمیق (شمع ها) عنوان ارائه : توسعه و کاربرد بانکهای اطلاعاتی پیهای عمیق Development and Applications of Databases in Deep Foundation Engineering By: Eslami & Moshfeghi

> ارائه دهنده: دکتر ابوالفضل اسلامی با همکاری مهندس سارا مشفقی ۱ آبان ۱۳۹۸ سالن همایش محل دائمی نمایشگاه های تخصصی شهر داری تهران



1	Data Sources in Geotechnical Engineering	منابع دادهها در مهندسی ژئوتکنیک
2	CPT, CPTu & Pile	آزمایش نفوذ مخروط و شمع
3	Recent Iranian Researches on CPT & Pile	<b>دستاوردهای اخیر محققین ایرانی: شمع و CPT</b>
4	<b>Overview of Some CPT &amp; Pile Databases</b>	<b>مرور بانکهای اطلاعاتی شمع و CPT</b>
5	Introduction to AUT;Geo-CPT&Pile Database	پایگاه دادههای ژئوتکنیکی دانشگاه صنعتی امیرکبیر
6	Typical Implementations	کاربردهای موردی
7	Concluding Remarks	جمع بندی نهایی

## 1. Sources of Data in GE

### Sources of Data:

- 1. Maps
- 2. Site visit
- 3. Drilling, boring, and sampling
- 4. Non-destructive tests (Geophysical tests)
- 5. On-situ tests
- 6. In-situ penetrating tests
- 7. Laboratory element testing
- 8. Laboratory physical modeling (model scale)
- 9. Full-scale testing
- **10. Instrumentation and Monitoring**







### 1. Sources of Data in GE



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### 1. Sources of Data in GE







### In-situ Testing vs. Laboratory Testing

#### Laboratory Tests Problems

- Difficulties in preparing undisturbed sample
- Soil disturbance
- Soil volume change
- Omitting confinement pressure
- Size effect and size limits

### In Situ Tests

- Overcome sampling difficulties
- Simple and fast
- Economical
- Generally applicable in foundation

engineering

آزمایشهای درجا و تستهای آزمایشگاهی: مکمل در مهندسی ژئوتکنیک

				Pa	irametei	rs and	specific	ations					
Applicability of in-situ tests	cation	profiling	sity, D <sub>r</sub>	çle, φ	shear	e, u	y, OCR	dulus	lity nd C <sub>c</sub>	n factors,	k	diagram	esistance
test	Soil classification	Vertical soil profiling	Relative density,	Friction angle,	Undrained shear strength, S <sub>u</sub>	Pore pressure,	Stress history, and K <sub>0</sub>	E <sub>s</sub> and G modulus	Compressibility factors, m <sub>v</sub> and	Consolidation factors, c <sub>v</sub> and c <sub>h</sub>	Permeability, k	Stress-strain diagram	Liquefaction resistance
Acoustic probe	С	в	в	С	С		С	С					С
Borehole permeability	С	<u> </u>	<u> </u>			Α				В	Α		
Cone (CPT)	[]	['											
Dynamic	С	Α	в	С	С		С						С
Electrical friction	в	A	в	С	в		С	в	С				в
Electrical piezocone	A	Α	в	в	в	Α	Α	в	в	Α	в	в	Α
Mechanical	в	A	в	С	в		С	в	С				в
Seismic down hole	С	С	С		<u> </u>			А				в	в
Dilatometer (DMT)	в	А	в	С	в		в	в	С			С	в
Hydraulic fracture	,	,			1	В	в			С	С		
Nuclear density tests (NDT)	,	·	А	в	,		1	С					
Plate load tests (PLT)	С	С	в	в	С		в	А	в	С	С	в	в
Pressure meter menard (PMT)	в	в	С	в	в		С	в	В			С	С
Self-boring pressure (SBPMT)	в	в	A	Α	Α	А	А	Α	А	Α	в	Α	А
Screw plate (SPLT)	С	С	в	С	в		в	А	В	С	С	в	в
Seismic down-hole	С	С	С		+ +		·	А				в	в
Seismic refraction (SR)	С	С			+		·	в					в
Shear vane (VST)	в	С	[]		A		в						
Standard penetration test (SPT)	в	в	в	С	С				С				А

A: high application B: medium application C:limited application

### 2. CPT, CPTu & Pile

### Cone Penetrometer (CPTu) Probes and Terminology

- ASTM D 5778 procedures
- No boring, No samples, No spoil
- Hydraulic Push at 20 mm/s
- Range of sizes:10 cm<sup>2</sup> and 15 cm<sup>2</sup> probes

#### **Advantages:**

- Fast and continuous profiling
- Repeatable and reliable
- Continuous records of  $q_c$ ,  $f_s$ , u per 2.5 cm
- Strong theoretical basis for interpretation

#### **Disadvantages:**

- High capital investment
- Requires skilled operators
- Limitation of use in gravel or cemented soils







### 2. CPT, CPTu & Pile

### Cone Tracks, Trucks and Special Rigs





















#### CPT & Pile Databases By: Eslami & Moshfeghi







#### **CPTu: Graphical Records and Log**





### **CPTu: Digital Records**

A	В	С	D	E	F	G	Н		
1			CPT DI	GITALS					
2	Z (m)	qc (MPa)	f <sub>s</sub> (MPa)	u <sub>2</sub> (MPa)	u <sub>0</sub> (MPa)	R <sub>f</sub> (%)	1		
3	0.0	0.237	0.000	0.007	0.000	0.000			
4	0.1	1.956	0.002	0.016	0.000	0.102			
5	0.2	4.859	0.031	0.070	0.000	0.633			
6	0.3	7.141	0.036	0.311	0.000	0.509			
7	0.4	8.681	0.067	0.047	0.000	0.771			
8	0.5	10.252	0.118	0.046	0.000	1.150			
9	0.6	8.593	0.104	0.013	0.000	1.208			
10	0.7	5.956	0.153	0.004	0.000	2.562			
11	0.8	4.919	0.145	0.003	0.000	2.940			
12	0.9	5.481	0.130	0.006	0.000	2.380			
13	1.0	6.548	0.112	0.007	0.000	1.718			
14	1.1	7.052	0.146	0.013	0.000	2.074			
15	1.2	8.830	0.168	0.013	0.000	1.900			
16	1.3	9.748	0.173	0.013	0.000	1.776			
17	1.4	10.252	0.202	0.013	0.000	1.972			
18	1.5	10.252	0.215	0.013	0.000	2.096			
19	1.6	11.052	0.246	0.019	0.000	2.227			
20	1.7	13.570	0.252	0.019	0.000	1.856			
21	1.8	12.948	0.316	0.046	0.000	2.438			
22	1.9	19.585	0.319	0.126	0.000	1.630			
23	2.0	32.119	0.168	0.086	0.000	0.524			
24	2.1	28.444	0.257	0.004	0.000	0.902			
25	2.2	19.970	0.464	0.189	0.000	2.322			

تولید حجم بسیار زیاد دادهها توسط CPT





#### **Special Piezocones**

- Resistivity Cone Penetration Test (RCPTu)
- Seismic Cone Penetration Test (SCPTu)
- Piezovibrocone
- Ultra violet induced fluorescence Cone Penetration Test (UVIF CPT)
- Dynamic Cone Penetration Test (DCPT)
- Cone Pressuremeter (CPMT)

UVIF (Volts) Rf % SBT U metres 0.0 12 150 0 50 3.0 0.0 5.0 0 Sensitive Fines **Clayey Silt** Silty Sand Sand Ultra Violet **Clayey Silt** Ē -10.0 Jun (Vo & Ve) **Clayey Silt** × -15.0 Sandy Silt Friction Sleeve (F. Sand **UVIF CPT Profile** Creosote Contaminated Zones







### **APPLICATIONS OF CPT IN GEOTECHNICAL ENGINEERING**







Penetrometer can be realized as a model pile.



# Bearing Capacity Direct CPT and CPTu-based methods: Pile Bearing Capacity

روشهای مبتنی بر CPT و CPT <b>u: تعیین</b>
ظرفیت باربری شمعها

No.	Method/ Reference	No.	Method/ Reference
1	Begemann (1963, 1965, 1969)	15	Fugro-05 (Kolk et al. 2005)
2	Meyerhof (1956, 1976, 1983)	16	UCD-05 (Gavin and Lehane 2005)
3	Aoki and Velloso (1975)	17	ICP-05 (Jardine et al. 2005)
4	Nottingham (1975), Schmertmann (1978)	18	UWA-05 (Lehane et al. 2005)
5	Penpile (Clisby et al.1978)	19	NGI-05 (Clausen et al. 2005)
6	Dutch (de Ruiter & Beringen 1979)	20	Cambridge-05 (White & Bolton 2005)
7	Philipponnat ( 1980)	21	Togiliani (2008)
8	LCPC (Bustamante & Gianeselli 1982)	22	German (Kempfert and Becker 2010)
9	Cone-m (Tumay & Fakhroo 1982)	23	UCD-11 (Igoe et al. 2010, 2011)
10	Price and Wardle (1982)	24	V–K (Van Dijk and Kolk 2011)
11	Gwizdala (1984)	25	SEU (Cai et al. 2011, 2012)
12	UniCone (Eslami & Fellenius 1997)	26	HKU (Yu and Yang 2012)
13	KTRI (Takesue et al. 1998)	27	UWA-13 (Lehane et al. 2013)
14	TCD-03 (Gavin and Lehane 2003)	28	Modified UniCone (Niazi and Mayne 2016)



#### CPT & Pile Databases By: Eslami & Moshfeghi

متد و نرم افزار UniCone

UniCone Program: Fellenius, Infante and Eslami (2002)

#### Pile Design (CPT/CPTu)

Soil Profiling (CPT/CPTu)

#### Input Data

**CPT/CPTu test results** 

**Pile Properties** 

**Soil Layers properties** 

<mark>#</mark> Import ASCII File: D:\!UniSoftI	niSoftUniSoft\UniCone\!UCN Manual\De 🔀
Column Delimiter	
Space Com	na Column Titles Row: 1
O Semi Colon 🛛 O Tab	Values Start at Row: 👖 🖨
☑ Treat consecutive delimit single	ers as a C CPT
	© CPTU net area ratio, a
Columns Containing Relevan	Data Proceed
Depth 1 m 🔹	ON <sup>f</sup> s 3 MPa -
□9c 2 MPa▼ □	u <sub>2</sub> 4 MPa • <u>C</u> ancel
File Contents	
UniCone	Manual 3 4 5 6 🔺
1 UniCone	Manual
2 Demo	xample for rofilin and pile
3 20.5	m lona 219 mm ised:▼ ▶



🕂 Pile Capacity Results: Eslan Toe Resistance

Depth

18.75 10.994

10 06 6 062

Depth qt

m

18.8

18.85

m

6.900

6.950

7.000

7.050

141 7 100 1 4

Shaft Resistance

1 2

3

137

138

139

140

qt MPa

9.427

8.020 18.9 7.223

MPa

1.7

1.5

1.5

1.4

- 1

**CPT & Pile Databases** By: Eslami & Moshfeghi

متد و نرم افزار UniCone

### **UniCone Program:** Fellenius, Infante and Eslami (2002

#### **Pile Capacity Calculation**

2)								
-)			UniCone		veic Doculto	Graphic Help		
			rile Iliput	COIC ANIA	ysis Results			
						CPT & Profiling		
						Pile Capacity	Eslami-Fellenius	Pile Capacity: Eslami-Fellenius
						Classification Chart	▶ Dutch	Unit Shaft
							LCPC	Resistance (KP a) Total Resistance (KN)
							Meyerhof	D 42 84 D 317 633 950
							Schmertmann	
mi Eol	lenius						_ 🗆 ×	
merei	ienius							
fs	u2					-	Unit Toe	
KPa	KPa						Resistance	
86.	150.1						11.00 MPa	
78.	150.3						Тое	
59.	150.						Resistance	
51.	152.6					-	409. KN	
10	454.0							
60		иE	20		Da	Soil Type	Total	
fs KPa	u2 KPa	qE MPa	CS	rs KPa	Rs KN	Soil Type 🔺	Shaft	$\left  \frac{1}{2} \right  $
n Pa 16.0	194.8	1.5	0.01	14.6		Silty Sand	Resistance	
16.0	194.0	1.3	0.01	32.6	144.1	Silty Clay	541.KN	
17.0	231.4	1.3	0.025	31.2		Silty Clay	,	
17.0	213.0	1.2	0.025	29.3	140.3	Silty Clay		
19.0 20.0	186.8	1.2	0.025	29.3		Silty Clay		
2.11				714	1211 1			
					Р	lie Capacity, R	u = 949.7KN	
						and and a second of the		

🛃 Summary			×
Method	Rt	Rs	R
Eslami-Fellenius	409. KN	541.KN	949.7KN Reset
European	376. KN	807.KN	1182.3KN Reset
LCPC	218. KN	340.KN	558.2KN Reset
Meyerhof	435. KN	223.KN	657.8KN Reset
Schmertmann	372. KN	411.KN	783.2KN Reset
Tumay	372. KN	442.KN	813.9KN Reset



### **UniCone Program:** Fellenius, Infante and Eslami (2002)

متد و نرم افزار UniCone

**CPT & Pile Databases** 

By: Eslami & Moshfeghi

Joh Proming	Soil	Profiling	
-------------	------	-----------	--

	Depth	qt	fs	u2	qE	Rf	Soil Type		
	m	MPa	KPa	KPa	MPa	%		]	
330	16.500	2.5	57.0	133.0	2.3	2.3	Silty Clay		
331	16.550	3.7	62.0	110.7	3.6	1.7	Silty Sand to Silt		(ba)
332	16.600	3.8	70.0	64.8	3.7	1.8	Silty Sand to Silt		q <sub>e</sub> (MPa)
333	16.650	5.1	52.0	83.2	5.0	1.0	Fine Sand and/or Silty Sand		ľ
334	16.700	6.8	54.0	12.2	6.8	0.8	Sand		
335	16.750	6.6	75.0	12.7	6.6	1.1	Fine Sand and/or Silty Sand		
336	16.800	5.8	127.0	1.4	5.8	2.2	Silty Sand to Silt		
337	16.850	3.6	114.0	24.0	3.6	3.2	Silty Sand to Silt		
338	16.900	2.8	82.0	76.1	2.7	2.9	Silty Clay		
339	16.950	3.2	95.0	90.5	3.1	3.0	Silty Clay	-	Ti Soil
340	17.000	2.8	66.0	92.4	2.7	2.4	Silty Clay		1000 -
341	17.050	4.3	44.0	114.3	4.2	1.0	Fine Sand and/or Silty Sand		8
342	17.100	5.6	63.0	39.8	5.6	1.1	Fine Sand and/or Silty Sand		star
343	17.150	6.0	77.0	41.8	6.0	1.3	Fine Sand and/or Silty Sand		100 - 20 20
344	17.200	7.0	75.0	59.1	6.9	1.1	Sand		Normalized Cone Resistance
345	17.250	7.4	76.0	45.7	7.3	1.0	Sand		
346	17.300	7.4	83.0	59.1	7.3	1.1	Sand		
347	17.350	8.5	88.0	83.5	8.4	1.0	Sand		orm
348	17.400	10.1	85.0	101.9	10.0	0.8	Sand		2





### Eslami Fellenius (1992-1996)-CGJ

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## Pile capacity by direct CPT and CPTu methods applied to 102 case histories

Abolfazl Eslami and Bengt H. Fellenius

Abstract: Six methods to determine axial pile capacity directly from cone penetration test (CPT) data are presented, discussed, and compared. Five of the methods are CPT methods that apply total stress and a filtered arithmetic average of cone resistance. One is a recently developed method, CPTu, that considers pore-water pressure and applies an unfiltered geometric average of cone resistance. To determine unit shaft resistance, the new method uses a new soil profiling chart based on CPTu data. The six methods are applied to 102 case histories combining CPTu data and capacities obtained in static loading tests in compression and tension. The pile capacities range from 80 to 8000 kN. The soil profiles range from soft to stiff clay, medium to dense sand, and mixtures of clay, silt, and sand. The pile embedment lengths range from 5 to 67 m and the pile diameters range from 200 to 900 mm. The new CPTu method for determining pile capacity demonstrates better agreement with the capacity determined in a static loading test and less scatter than by CPT methods.

Key words: cone penetration test, pile capacity, toe resistance, shaft resistance, soil classification.

ظرفیت باربری محوری شمعها با استفاده از نتایج CPT و CPTu

**CPT & Pile Databases** 

By: Eslami & Moshfeghi

طبقهبندی رفتاری خاکها (SBC)







**CPT & Pile Databases By: Eslami & Moshfeghi** 



### ظرفیت باربری محوری شمع ها با استفاده از نتایج CPTu

Scale Effects





CPT & Pile Databases By: Eslami & Moshfeghi

#### Eslami & Gholami (2003, 2006)

Scientia Iranica, Vol. 13, No. 3, pp 223–233 © Sharif University of Technology, July 2006

#### Analytical Model for the Ultimate Bearing Capacity of Foundations from Cone Resistance

#### A. Eslami<sup>\*</sup> and M. Gholami<sup>1</sup>

By application of Cone Penetration Test (CPT) data for shallow foundation (footing) design, the problems of providing representative undisturbed samples and, rather,  $\varphi - N$  coefficient relations will be eliminated. An analytical model, based on a general shear failure mechanism of the logarithm spiral type, has been developed for calculating, directly, bearing capacity of footings,  $q_{ult}$  from cone resistance,  $q_c$ . The transform of the failure in channel from a shallow to a deep foundation and the scale effect have been considered in the proposed in ethod. Six current CPT direct methods for determining the bearing capacity of nutrings we been investigated. The proposed method and others were compared to the method space, ranging from 1.7 to 15 kg/cm<sup>2</sup>, of 28 footings compiled in a database with a range on "ameter from 0.3 to 3 m located in different soils. The graphical and cumulative proposed set we approaches for the validation of the methods indicates optimistic results for the bearing capacity estimation of the proposed method, which is simple and routine.

**ظرفیت باربری پی ها با استفاده از نتایج CPTu** 





#### Shariatmadari, Eslami & KarimpourFard (2008)

Iranian Journal of Science & Technology, Transaction B, Engineering, Vol. 32, No. B2, pp 125-140 Printed in The Islamic Republic of Iran, 2008 © Shiraz University

#### BEARING CAPACITY OF DRIVEN PILES IN SANDS FROM SPT-APPLIED TO 60 CASE HISTORIES<sup>\*</sup>

#### N. SHARIATMADARI<sup>1\*\*</sup>, A. ESLAMI<sup>2</sup> AND M. KARIMPOUR-FARD<sup>1</sup>

<sup>1</sup>Dept. of Civil Eng., Iran University of Science and Technology, Tehran, I. R. of Iran Email: Shariatmadari@iust.ac.ir <sup>2</sup>Dept. of Civil Eng., Guilan University, Rasht, I. R. of Iran

Abstract- In recent years determining bearing capacity of piles from in-situ testing data as a complement of static and dynamic analysis has been used by geotechnical engineers. In this paper, different approaches for estimating the bearing capacity of piles from SPT data have been explained and compared. A new method based on the N-value from SPT is presented and calibrated. Data averaging, failure zone extension, and plunging failure of piles has been noticed in the proposed approach. A data base has been compiled including 43 full scale static pile load tests and 17 dynamic testings which were analyzed with the signal matching technique by CAPWAP. The SPT data were performed close to pile locations are also included in the data base. A comparison of current methods by error investigation with cumulative probability and Log-Normal approaches demonstrates that the proposed method predicts pile capacity with more accuracy and less scatter than other methods. Results of prediction with good agreement to measured capacities indicate that the proposed method can be used as an alternative for determining the bearing capacity of piles in geotechnical practice.

Keywords- Pile, bearing capacity, standard penetration test, SPT, static and dynamic load tests

CPT & Pile Databases By: Eslami & Moshfeghi

ظرفیت باربری شمع های کوبشی در ماسه با استفاده از نتایج CPT، SPT و موارد عملی



#### Ahmadi, Byrne and Campanella (2011)

## Cone tip resistance in sand: modeling, verification, and applications

M.M. Ahmadi, P.M. Byrne, and R.G. Campanella

Abstract: A numerical modeling procedure is presented to evaluate cone tip resistance in sand. The procedure involves a moving boundary simulating cone penetration. The soil is modeled as a Mohr–Coulomb elastic–plastic material with stress-dependent parameters. The procedure is verified by comparing predicted numerical values of cone tip resistance with published experimental measurements from calibration chamber tests. The selected database consists of 59 calibration chamber tests on Ticino sand with different relative densities, overconsolidation ratios, stresses, and boundary conditions. Several applications of the modeling procedure are also presented. The computer program FLAC is used to carry out the analysis.

Key words: cone tip resistance, numerical modeling, sand, calibration chamber, Mohr-Coulomb, in situ horizontal stress.

**Résumé :** On présente une procédure de modélisation pour évaluer la résistance de pointe du cône dans le sable. La procédure implique une frontière mobile simulant la pénétration du cône. Le sol est modélisé comme un matériau élasto-plastique Mohr–Coulomb avec des paramètres dépendant des contraintes. La procédure est vérifiée en comparant les valeurs numériques prédites de la résistance de pointe du cône avec les mesures expérimentales publiées d'essais en chambre de calibrage. La banque de données choisie comprend 59 essais en chambre de calibrage sur le sable de Ti-cino avec des valeurs différentes de densités, d'OCR, de contraintes et de conditions aux frontières. On présente aussi plusieurs applications de procédures de modélisation. Le programme d'ordinateur FLAC est utilisé pour réaliser l'analyse.

Mots clés : résistance à la pointe du cône, modélisation numérique, sable, chambre de calibrage; Mohr-Coulomb, contrainte horizontale in situ. **CPT در ماسه:** \* مدلسازی \* صحت سنجی \* کاربرد

[Traduit par la Rédaction]



Ahmadi and Robertson (2008)

Scientia Iranica, Vol. 15, No. 5, pp 541-553 © Sharif University of Technology, October 2008

> A Numerical Study of Chamber Size and Boundary Effects on CPT Tip Resistance in NC Sand

> > M.M. Ahmadi<sup>1,\*</sup> and P.K. Robertson<sup>2</sup>

A numerical modeling procedure was used to quantify calibration chamber size and boundary effects for cone penetration testing in sand. In the numerical analyses, chamber diameter and boundary conditions were varied to investigate the effects of chamber size and boundary conditions on cone tip resistance. These analyses show that, for loose sand, a chamber-to-cone diameter ratio of 33 is sufficient for the boundaries to have no influence on the cone tip measurements. However, for very dense sand, the numerical analyses show that the chamber-to-cone diameter ratio should be more than 100 to ensure that boundaries have no influence on cone tip measurements. Numerical analysis indicates that, not only the sand relative density but its stress state is also a significant factor in influencing the chamber size effects. The results of the numerical analyses were compared to existing empirically based relationships. Suggestions are provided to reduce the effects of chamber size and boundaries on cone tip resistance measurements in sand.

**CPT & Pile Databases By: Eslami & Moshfeghi** 

S C I E N T I A I R A N I C A





### 3. Recent Iranian Researches on CPT & Pile

Ahmadi and Robertson (2008)

### مطالعه عددی اثر شرایط مرزی و سایز محفظه بر نتایج CPT





### Eslami, Tajvidi & Karimpour Fard (2013)



International Journal of Civil Engineering

Geotechnical Engineering

## Efficiency of methods for determining pile axial capacity-applied to 70 cases histories in Persian Gulf northern shore

**A. Eslami<sup>1,\*</sup>, I. Tajvidi<sup>2</sup>, M. Karimpour-Fard<sup>3</sup>** Received: July 2012, Revised: December 2012, Accepted: January 2013

#### Abstract

Three common approaches to determine the axial pile capacity based on static analysis and in-situ tests are presented, compared and evaluated. The Unified Pile Design (UPD), American Petroleum Institute (API) and a SPT based methods were chosen to be validated. The API is a common method to estimate the axial bearing capacity of piles in marine environments, where as the others are currently used by geotechnical engineers. Seventy pile load test records performed in the northern bank of Persian Gulf with SPT profile have been compiled for methods evaluation. In all cases, pile capacities were measured using full scale static compression and/or pull out loading tests. As the loading tests in some cases were in the format of proof test without reaching the plunging or ultimate bearing capacity, for interpretation the results, offset limit load criteria was employed. Three statistical and probability based approaches in the form of a systematic ranking, called Rank Index, RI, were utilized to evaluate the performance of predictive methods. Wasted Capacity Index (WCI) concept was also applied to validate the efficiency of current methods. The evaluations revealed that among these three predictive methods, the UPD is more accurate and cost effective than the others.

Keywords: Pile, Axial Bearing Capacity, Full scale load test, Predictive methods efficiency, Wasted capacity index (WCI).





### 3. Recent Iranian Researches on CPT & Pile



کارایی روش های تعیین ظرفیت باربری با استفاده از مـوارد عملـی در ناحیـه شمالی خلیج فارس (WCl)



Typical case pile load test and SPT test result in Khalij-e Fars Ship Yard project



### Eslami, Aflaki & Hosseini (2008-2011)



Sharif University of Technology

Scientia Iranica Transactions A: Civil Engineering www.sciencedirect.com

Evaluating CPT and CPTu based pile bearing capacity estimation methods using Urmiyeh Lake Causeway piling records

#### A. Eslami<sup>a</sup>, E. Aflaki<sup>a,\*</sup>, B. Hosseini<sup>b</sup>

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Received 23 May 2010; revised 1 June 2011; accepted 21 August 2011

#### KEYWORDS

Pile bearing capacity; CPT and CPTu methods; Dynamic testing; Urmiyeh Lake Causeway. Abstract Urmiyeh Lake is the largest super salt water situated in the north-west of Iran. A causeway embankment has been constructed in the narrowest part of the lake from both sides about 13.5 km, in order to connect two provincial capital cities of Tabriz and Urmiyeh of eastern and western Azerbaijan provinces to Europe through Turkey, while a 1280 m opening in between linked up by a bridge. Based on soil classification methods, utilizing CPTu data and soil sampling, the lake sediments consist of 150 m of soft and very sensitive clay. In order to evaluate the bearing capacity of driven piles of the bridge, eight long steel piles with diameters of 813 and 66 m and lengths of 75 m have been instrumented and monitored based on static and dynamic load testing program. Piezocone (CPTu) results are also available from adjacent pile locations. Results of pile capacity calculation based on direct CPT and CPTu methods demonstrate that reasonable accuracy can be achieved in reference to dynamic testing. Therefore, combination of CPTu data with dynamic testing results can be considered by engineers for predicting bearing capacity of piles in offshore and bridge structures, where the static pile load testing is difficult, time consuming and expensive in marine environment.

© 2011 Sharif University of Technology. Production and hosting by Elsevier B.V. Open access under <u>CC BY license</u> ارزیابی ظرفیت بساربری شسمع هسای پسل میانگذر دریاچه ارومیه با استفاده از نتسایج CPTu

CPTu the major source of subsoil data in this project.

CPTu soundings were performed in 12 locations, down to 100 m below the lake-bed.

### **Super Soft Deposits**



### 3. Recent Iranian Researches on CPT & Pile





ارزیابی ظرفیت بساربری شسمع های پل میانگذر دریاچه ارومیه **با استفاده از نتایج CPTu** 





### Asghari, Habibagahi, Ghahramani, Fakharian (2019)

International Journal of Civil Engineering https://doi.org/10.1007/s40999-019-00443-0

**RESEARCH PAPER** 

#### Reliability-Based Calibration of Resistance Factors in LRFD Method for Driven Pile Foundations on Inshore Regions of Iran

 $Seyed \ Ali \ Asghari \ Pari^1 \cdot Ghassem \ Habibagahi^1 \cdot Arsalan \ Ghahramani^1 \cdot Kazem \ Fakharian^2$ 

Received: 21 January 2019 / Revised: 23 May 2019 / Accepted: 25 May 2019 © Iran University of Science and Technology 2019

#### Abstract

This paper presents the improvement of load and resistance factor design (LRFD) method for axially loaded driven piles in Iran. The LRFD method has been well developed and successfully implemented in geotechnical engineering, especially in the design of pile foundations in different parts of the world. To extend the use of this method in Iran, it is necessary to use the results of reliable local pile load tests and construction records to calibrate LRFD resistance factors regionally. To this end, we first collected a comprehensive database of static and dynamic load tests which have been performed on driven piles in fine-grained soils across Iran. Based on this database, we calculated the resistance factors for different design methods using three different methods of reliability analysis (FORM, FOSM, and MCS) and for two levels of reliability ( $\beta_T$ =2.33 and 3). Finally, we used these calculations together with experience and engineering judgment to propose resistance factors for the National Building Code of Iran.

Keywords LRFD · Code calibration · Reliability analysis · Pile foundation design



Check for

به روش LRF**D؛ شــمعهـا**; کوبشی نواحی ساحلی ایران



#### Fakharian & Khanmohammadi (2018)

Comparison of Pile Bearing Capacity from CPT and Dynamic Load Tests in Clay Considering Soil Setup

K. Fakharian, M.R. Khanmohammadi Amirkabir University of Technology, Tehran, Iran ظرفیت باربری شمع با استفاده از CPT و آزمایش بارگذاری دینامیکی در رس با لحاظ اثر گیرش خاک

**CPT & Pile Databases** 

By: Eslami & Moshfeghi

ABSTRACT: The CPT direct methods are vastly used to estimate the pile tip and shaft resistances in many piling projects. In driven piles embedded in clay, "soil setup" phenomenon is understood to be contributing to increase the pile bearing capacity and in particular the shaft resistance component with time. Considering "time effects" on pile shaft resistance, the question arises that how accurately CPT-based methods could estimate the bearing capacity of piles? The main objective of this paper is to compare the CPT capacity predictions with those resulted from pile Dynamic Load Tests (DLT) at End-Of-Drive (EOD) and Beginning-Of-Restrike (BOR) as well as Static Load Tests (SLT). The focus of this study has been on the field results of four "test piles" driven in North Azadegan Oilfield in Khuzestan Province, Iran. The test results show that almost all CPT-based methods have ended up in higher capacity predictions compared to EOD capacities, but generally lower than the BOR capacities. The findings of the study are useful in engineering application of offshore piling in clay deposits in which the time constraints of construction does not allow performance of dynamic load tests at different time steps. Also, setting up static load test is not feasible in such environments to measure the setup effects.



#### Baziar, Kashkooli, Saeedi Azizkandi (2012)



Computers and Geotechnics 45 (2012) 74-82

**Computers and Geotechnics** 

Contents lists available at SciVerse ScienceDirect

journal homepage: www.elsevier.com/locate/compgeo



Mohammad Hassan Baziar<sup>a,\*</sup>, Armin Kashkooli<sup>b</sup>, Alireza Saeedi-Azizkandi<sup>b</sup>

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#### ARTICLE INFO

Article history: Received 12 September 2011 Received in revised form 5 March 2012 Accepted 17 April 2012 Available online 1 June 2012

Keywords: Pile shaft resistance Neural network Non-linear multi regression Cone penetration test ABSTRACT

Accurately predicting pile shaft resistance when designing pile foundations is necessary for ensuring appropriate structural and serviceability performance. The scope of this research includes four main components: (I) compiling shaft resistance datasets obtained from the published literature; (II) developing two artificial neural network (ANN) and non-linear multi regression models for predicting pile shaft resistance using cone penetration test (CPT) results; (III) investigating the influence of input parameters on the resulting shaft friction and their degrees of importance; and (IV) assessing the relative accuracies of the presented models using a number of traditional methods. It is quantitatively demonstrated that the ANN and non-linear multiple regression models proposed in the current study out perform the traditional methods and can be used by engineers to accurately predict pile shaft resistance.

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#### Saeedi Azizkandi, Kashkooli & Baziar (2014)

Geotech Geol Eng (2014) 32:1043–1052 DOI 10.1007/s10706-014-9779-y

ORIGINAL PAPER

#### **Prediction of Uplift Pile Displacement Based on Cone Penetration Tests (CPT)**

#### A. Saeedi Azizkandi · A. Kashkooli · M. H. Baziar

Received: 8 April 2012/Accepted: 17 May 2014/Published online: 25 May 2014 © The Author(s) 2014. This article is published with open access at Springerlink.com

Abstract Accurate prediction of uplift pile displacement is necessary to ensure appropriate structural and serviceability performance of civil projects. On the other hand, in recent years, machine-learning models have been applied to many geotechnical-engineering problems, with some degrees of success. The scope of this research includes three main stages: (1) the compilation of load-displacement data sets, obtained from the published literature, (2) analysis of machine learning models that predict the uplift pile displacement based on the cone penetration test data, and the relative importance of input parameters that have been evaluated using senility analysis by the artificial neural network, In addition, this paper also examines the different selection of input parameters and internal network parameters to obtain the optimum model, (3) A parametric study has also been performed for the input parameters to study the consistency of the suggested model. The statistical parameters and parametric study obtained in this research show the superiority of the current model. It is demonstrated that machine learning models such as ANN and GP models outperform the traditional methods, and provide accurate uplift pile displacement predictions.

Keywords Uplift pile · Displacement · Cone penetration tests · Artificial neural network (ANN) · Genetic programming (GP)

#### 1 Introduction

Pile foundations are used to transmit the superstructure load to deeper strata, when the subsurface soil is of inadequate strength. Pile foundations are often subjected to axial and lateral loads. Under the action of lateral loads and moments, some of the piles in a group, may experience uplift displacement. In compressive loading, the tip resistance of piles plays a major role in pile capacity. In contrast to the compressive loading situation, the shaft resistance capacity alone works against the piles uplift force. On the other the hand, the tensile strength of soil is quite some hand the strength of soil is quite

### تخمین جابجایی شمع تحت بـار کششی با استفاده از CPT

**CPT & Pile Databases** 

By: Eslami & Moshfeghi



### Ebrahimian & Movahed (2016)

Ships and Offshore Structures, 2016 http://dx.doi.org/10.1080/17445302.2015.1116243

Taylor & Francis Taylor & Francis Croup



#### Application of an evolutionary-based approach in evaluating pile bearing capacity using CPT results

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<sup>a</sup>Faculty of Civil, Water and Environmental Engineering, Abbaspour School of Engineering, Shahid Beheshti University (SBU), Tehran, Iran; <sup>b</sup>The Highest Prestigious Scientific and Professional National Foundation, Iran's National Elites Foundation (INEF), Tehran, Iran; <sup>c</sup>School of Civil Engineering, Iran University of Science and Technology, Tehran, Iran

(Received 3 November 2014; accepted 31 October 2015)

Predicting ultimate axial bearing capacity of pile foundations is an important and complicated problem in geotechnical engineering. Cone penetration test (CPT) is a reliable *in situ* test widely used in the analysis and design of pile foundations. In this study, new CPT-based axial pile bearing capacity models are presented for both cohesionless and cohesive soils using evolutionary polynomial regression (EPR), a branch of evolutionary approaches. A relatively comprehensive database is gathered and divided into training and testing sub-sets to avoid over-fitting. This database includes both coarse and fine grain soils, cone tip resistance and sleeve friction of CPTs, geometry and bearing capacity of piles. The presented models are compared to some previously published ones and their preferences are demonstrated statistically and probabilistically. Proper applicability of the models in predicting axial pile bearing capacity is then confirmed by field verification, compared to analytical and empirical models available in the literature.

Keywords: pile foundation; bearing capacity; cone penetration test; evolutionary polynomial regression; statistical analysis


## 3. Recent Iranian Researches on CPT & Pile

### **CPT & Pile Databases** By: Eslami & Moshfeghi

### Ardalan, Eslami & Nariman-Zadeh (2008)



Contents lists available at ScienceDirect

Computers and Geotechnics



journal homepage: www.elsevier.com/locate/compgeo

### Piles shaft capacity from CPT and CPTu data by polynomial neural networks and genetic algorithms

H. Ardalan<sup>a</sup>, A. Eslami<sup>b,\*</sup>, N. Nariman-Zadeh<sup>c</sup>

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#### ARTICLE INFO

Article history: Received 14 May 2008 Received in revised form 16 September 2008 Accepted 16 September 2008 Available online 4 November 2008

Keywords: Pile shaft capacity Cone penetration test (CPT) Piezocone (CPTu) Neural networks GMDH Genetic algorithm

#### ABSTRACT

Cone penetration test (CPT) is one of the most common in situ tests which is used for pile design because it can be realized as a model pile. The measured cone resistance  $(q_c)$  and sleeve friction  $(f_s)$  usually are employed for estimation of pile unit toe and shaft resistances, respectively. Thirty three pile case histories have been compiled including static loading tests performed in uplift, or in push with separation of shaft and toe resistances at sites which comprise CPT or CPTu sounding. Group method of data handling (GMDH) type neural networks optimized using genetic algorithms (GAs) are used to model the effects of effective cone point resistance  $(q_E)$  and cone sleeve friction  $(f_s)$  as input parameters on pile unit shaft resistance, applying some experimentally obtained training and test data. Sensitivity analysis of the obtained model has been carried out to study the influence of input parameters on model output. Some graphs have been derived from sensitivity analysis to estimate pile unit shaft resistance based on  $q_E$  and fs. The performance of the proposed method has been compared with the other CPT and CPTu direct methods and referenced to measured piles shaft capacity. The results demonstrate that appreciable **Experimental and predicted unit shaft capacities** 

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A generalized GMDH network structure of chromosome.





## 3. Recent Iranian Researches on CPT & Pile

Veiskarami, Eslami & Kumar (2010-2011)

1570

End-bearing capacity of driven piles in sand using the stress characteristics method: analysis and implementation

Mehdi Veiskarami, Abolfazl Eslami, and Jyant Kumar

Abstract: The method of stress characteristics has been employed to compute the end-bearing capacity of driven piles. The dependency of the soil internal friction angle on the stress level has been incorporated to achieve more realistic predictions for the end-bearing capacity of piles. The validity of the assumption of the superposition principle while using the bearing capacity equation based on soil plasticity concepts, when applied to deep foundations, has been examined. Fourteen pile case histories were compiled with cone penetration tests (CPT) performed in the vicinity of different pile locations. The end-bearing capacity of the piles was computed using different methods, namely, static analysis, effective stress approach, direct CPT, and the proposed approach. The comparison between predictions made by different methods and measured records shows that the stress-level-based method of stress characteristics compares better with experimental data. Finally, the end-bearing capacity of driven piles in sand was expressed in terms of a general expression with the addition of a new factor that accounts for different factors contributing to the bearing capacity. The influence of the soil nonassociative flow rule has also been included to achieve more realistic results.

Key words: bearing capacity, cone penetration tests, failure, friction angles, piles, plasticity.

**CPT & Pile Databases By: Eslami & Moshfeghi** 

ظرفیت باربری کف شمع کوبشی در ماسه با استفاده از روش مشخصه تنش



Boundary conditions of Bolton and Lau (1993) with a straight rigid cone نگرش نوین بر طراحی و اجرای یی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸



CPT & Pile Databases By: Eslami & Moshfeghi

کف شمع کوبشی در ماسه

## 3. Recent Iranian Researches on CPT & Pile

Veiskarami, Eslami & Kumar (2010-2011)



### Stress characteristics and variation of soil friction angle at failure



## 3. Recent Iranian Researches on CPT & Pile

## Eslami & Mohammadi (2016)

Ships and Offshore Structures, 2016 http://dx.doi.org/10.1080/17445302.2015.1131082





### Drained soil shear strength parameters from CPTu data for marine deposits by analytical model

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(Received 11 January 2015; accepted 8 December 2015)

Soil shear strength parameters, i.e. cohesion (C) and friction angle ( $\varphi$ ) are typically determined using laboratory and *in situ* tests, although some limitations are involved in laboratory tests, such as the need for considering size effects and the use of undisturbed sampling. Cone penetration testing (CPT) has been recognised as a rapid and versatile procedure to provide continuous soil records, particularly in marine environment. In this study, an analytical approach is utilised to calculate drained soil strength parameters using piezocone penetration test (CPTu) records, i.e.  $q_t$  (corrected point resistance) and  $f_s$  (sleeve friction) and the results are compared with those obtained from laboratory tests. Current methods for obtaining shear strength parameters using CPT data are based on bearing capacity and cavity expansion theories and are able to estimate only  $\varphi$  in sands, and undrained shear strength ( $S_u$ ) in cohesive soils. In this paper, by combining bearing capacity theories and direct shear modes of failure at CPTu tip and sleeve resistances, and considering the pore water pressure at the shoulder of the piezocone ( $u_2$ ), a set of equations is derived. By inputting CPTu data including  $q_t$ ,  $f_s$  and  $u_2$  at a certain depth, soil shear strength parameters can be calculated simultaneously. Finally results obtained from this method are compared with measured soil shear strength parameters, using a data bank consisting of 50 sets of CPTu sounding carried out in marine deposits at various locations around the world. The comparison between predicted and measured *C* and  $\varphi$  values indicates good consistency and low scatter for the results obtain from the proposed method. This demonstrates that the proposed method is able to predict soil shear strength parameters in difficult marine environments with acceptable accuracy.

Keywords: shear strength parameters; CPTu; marine deposits; analytical approach



CPT & Pile Databases By: Eslami & Moshfeghi

## 3. Recent Iranian Researches on CPT & Pile

یارامترهای مقاومت برشی زهکشی شده خاک ؛ Eslami & Mohammadi (2016) **با استفاده از رکوردهای CPTu در نهشته های دریایی** Input Data Output C', φ'  $q_{c}, f_{s}, u_{2}$  $\left| C + 0.000789(1 - \sin\phi)\sigma_{\nu_0}' \tan\left(\frac{2}{3}\phi\right) \left[ \frac{q_c - \left(\frac{\sigma_{\nu_0} - 2\sigma_{h_0}}{3}\right)}{\left(\frac{\sigma_{\nu_0}' - 2\sigma_{h_0}'}{2}\right)} \right]^{1.44} = f_s$  $\left(\tan^2\left(\frac{\pi}{4}+\frac{\Phi}{2}\right)e^{\pi tan\Phi}-1\right)C \cot\Phi+\overline{q}.\tan^2\left(\frac{\pi}{4}+\frac{\Phi}{2}\right)e^{\pi tan\Phi}+$  $\gamma B \left[ tan^2 \left( \frac{\pi}{4} + \frac{\Phi}{2} \right) e^{\pi tan\Phi} + 1 \right] tan\Phi = q_E + N_u \Delta U$ 



## 3. Recent Iranian Researches on CPT & Pile

**CPT & Pile Databases By: Eslami & Moshfeghi** 

### Fateh, Eslami & Fahimifar (2015)

باربری شمع های پیچشی پره ای با استفاده از نتایج CPT

MARINE GEORESOURCES & GEOTECHNOLOGY http://dx.doi.org/10.1080/1064119X.2015.1133741

### Direct CPT and CPTu methods for determining bearing capacity of helical piles

Amir Mansour Askari Fateh, Abolfazl Eslami, and Ahmad Fahimifar

Department of Civil and Environmental Engineering, Amirkabir University of Technology (AUT), Tehran, Iran

#### ABSTRACT

Helical piles are structural deep foundation elements, which can be categorized as torgue-driven piles without any limitations to implement in marine situations. Different methods are used to predict the axial capacity of helical piles, such as static analysis, but have some limitation for this type of piles on marine conditions. In situ testing methods as supplement of static analysis have been rarely used for helical piles. In geotechnical engineering practice, the most common in situ tests particularly applicable for coastal or offshore site investigation are cone penetration test (CPT) and piezocone penetration test (CPTu). The CPT is simple, repeatable, and prepares the continuous records of soil layers. In this paper, a data bank has been compiled by collecting the results of static pile load tests on thirty-seven helical piles in ten different sites including CPT or CPTu data. Axial capacities of thirty-seven helical piles in different sites were predicted by direct CPT methods and static analysis. Accuracy estimation of ten direct CPT methods to predict the axial capacity of helical piles was investigated in this study. Comparisons have been made among predicted values and measured capacity from the pile load tests. Results indicated that the recently developed methods such as NGI-05 (2005), ICP-05 (2005), and UWA-05 (2005) predicted axial capacity of helical piles more accurately than the other methods such as Meyerhof (1983), Schmertmann (1978), Dutch (1979), LCPC (1982), or Unicone (1997). However, more investigations are required to establish better correlation between CPT data and axial capacity of helical piles.

Taylor & Francis Taylor & Francis Group

ARTICLE HISTORY

2015

analysis

**KEYWORDS** 

Received 28 September

2015 Accepted 15 December

Bearing capacity; direct CPT

and CPTu methods: helical

pile; pile load test; static





نگرش نوین بر طراحی و اجرای پی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸



## 3. Recent Iranian Researches on CPT & Pile

### **CPT & Pile Databases By: Eslami & Moshfeghi**

Eslami, Moshfeghi, Mollabasi & Eslami M. (2019)

## **Piezocone and Cone Penetration Test Applications** in Foundation Engineering

- **Ch. 1: Geotechnical Engineering**
- **Ch. 2: Foundation Engineering**
- **Ch. 3: CPT Records and Performance**
- **Ch. 4: Geotechnical Parameters from CPT Records**
- Ch. 5: Soil Behavior Classification (SBC) Using CPT and CPTu Records
- Ch. 6: Scale Effect and CPTu Applications for Shallow Foundations
- Ch. 7: CPT & CPTu Applications for Deep Foundation Bearing Capacity
- Ch. 8: CPT & CPTu: Settlement Estimation
- Ch. 9: Soil improvement
- Ch. 10: GMDH and Soft Computing
- Ch. 11: Uncertainty and Reliability Based Approaches
- Ch. 12: Case Histories and Database



## Piezocone Penetration and Cone Test Application In Foundation Engineering

BH

Abolfazi Eslami, Mohammad M. Eslami, Hossein Molaabasi, Sara Moshfeghi



# **Databases**

- Databases are collections of data which are organized in order to facilitate access and retrieving data when they are needed.
- Examples of Databases in Geotechnical Engineering:
  - 1. Pile loading test
  - 2. Pile loading test under lateral load
  - 3. Retaining walls and displacement due to deep excavation
  - 4. In-situ tests
  - 5. Specifications of geotechnical boreholes
  - 6. Settlement of shallow foundations

پایگاه داده یا بانک اطلاعاتی: مجموعهای از دادههای سازمان دهی شده به نحسوی

که در مواقع نیاز به آسانی در دسترس، مورد بازیابی و شبیهسازی قرار گیرند.



# Databases

## **Advantages and Applications:**

- I. Cost saving and project execution time
- II. Optimization of design methods
- III. Evaluation of design methods
- IV. Development of new methods
- V. Improvement of geotechnical studies



## **Berkeley Liquefaction Investigation**

## □ Records of earthquakes:

- ✓ Adapazari (1999) in Turkey
- ✓ Chi Chi (1999) in Taiwan
- □ Records of CPT and SPT
- □ Investigation of liquefied
  - soils during earthquake





## 4. Overview of Some CPT & Pile Databases

## **USGS Earthquake Hazards Program**

All Regions

Arkansas

**Red River** 

**Ouachita River** 

California (Northern)

Alameda County

Monterey County

San Francisco County

San Mateo County

Santa Clara County

Mono County

CPT records performed all over the North America

1500+ tests carried out from 1979 to 2011

Seismic investigation and soil liquefaction assessment

Science for a changing world	
------------------------------	--

### Table of CPT Data

### All Regions

Sounding	Download	Date	Depth (m)	Longitude	Latitude	V,30 (m/s)
SCC136	Adobe .pdf   ASCII .txt	1975-05-05	10.4	-121.9257	37.41068	
SMC019	Adobe .pdf   ASCII .txt	1978-05-17	180	-122.13181	37.49645	
SMC024	Adobe .pdf   ASCII .txt	1979-06-25	9	-122.45215	37.67183	
SMC025	Adobe .pdf   ASCII .txt	1979-06-25	9.2	-122.45213	37.67182	
SMC026	Adobe .pdf   ASCII .txt	1979-06-25	8.8	-122.45216	37.67182	
SMC027	Adobe .pdf   ASCII .txt	1979-07-03	13	-122.4335	37.65504	
SMC028	Adobe .pdf   ASCII .txt	1979-07-03	12.2	-122.43352	37.65504	
SMC029	Adobe .pdf   ASCII .txt	1979-07-03	12.4	-122.43349	37.65504	

### نگرش نوین بر طراحی و اجرای پی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸



## Iowa State University Database-PILOT (Roling et al., 2011)

□ Comprising both static and dynamic data for driven piles back to 1966

□ 274 piles of various shapes driven within the state of lowa

□ Establishment of resistance factors for LRFD and a reliable construction-control method for

		Data Versio		or Plle	LDad To Updated on	ests (PILO 02/10/2011	IT)	OF S	CIENCE AND		
	-	New P	ile Load Test	About	Filter Favorite	5	-	Techn A Daveso	ology Burea Force or Inscharts	IOWA HIGHW	
		ID +1	County •	Township •	Lab Number •	Project Number ·	Design Num •	Contractor •	Pile Type •	Design Load •	Date Drive
		1	Black Hawk	Orange	AXP3-7	IY-520-6(8)3P-07	1983	Lunda Construc	HP 10 X 42	32	12/9/198
		2	Johnson	Clear Creek	AXP3-9	1-380-6(44)24301-52	ł	A. M. Cohron &	HP 10 X 42	34	6/15/197
		3	Fremont		AXP3-10	FN-184-1(3)21-36	173	A. M. Cohron &	HP 10 X 42	37	7/24/197
	-	4	Jones		AXP3-14	FM-38-3(7)21-53	170	Grimshaw Con:	HP 10 X 42	37	8/21/197
		5	Jasper	Malaka	AXP4-2	BROS-9050(2)8J-50	383	Herberger Con	HP 10 X 42	31	5/23/198
		6	Decatur	Center	AXP4-3	BRF-2-5(10)38-27	1082	Godberson - Sr	HP 10 X 42	35	6/18/198
		Z	Cherokee	Afton	AXP4-6	BRF-3-2(20)38-18	683	Christensen Br	HP 10 X 42	35	11/21/198
$\sim$		8	Linn	Rapids	AXP4-22	I-IG-380-6(57)25904	1672	Schmidt Constr	HP 10 X 42	37	8/7/1974
		0	Linn	Rapids	AXP4-23	1-1G-380-6(57)25904	1672	Schmidt Constr	HP 10 X 42	37	11/14/197

driven piles



## 4. Overview of Some CPT & Pile Databases

## Driven Pile Ground Vibration Case History (Hajduk et al., 2009)

 An important first step towards future examining of the environmental effects of pile driving on adjacent structures and residents

Incorporates available data from the technical literature and data provided by professionals within the pile driving industry

### **CPT & Pile Databases By: Eslami & Moshfeghi**

Case No. <sup>1</sup>	Location	Pile Size	Hammer Type	Hammer	Data Points
1	Charleston SC	HP305x79 (HP12x53)	Hydraulic	ICE 75	203
1	Charleston, SC	30.5cm (12in) OEP	Hydraulic	ICE 75	7
2	Charleston, SC	30.5cm (12in) PSC	Hydraulic	ICE 75	396
3	Sullivan's Is., SC	20.3cm (8in) Timber	Air	Vulcan 6 ECH	108
4	Isle of Palms, SC	25.4cm (10in) Timber	Air	Vulcan 06	56
ę	Charlester SC	25.4cm (10in) PSC	Hydraulic	ICE 115	35
5	Charleston, SC	30.5cm (12in) PSC	Hydraulic	ICE 115	72
6	Charleston, SC	HP305x79 (HP12x53)	Air	Vulcan 01	9
		HP305x79 (HP12x53)	Vibratory	APE 200	22
7	Charleston, SC	AZ 13	Vibratory	APE 200	71
		AZ 18	Vibratory	APE 200	28
8	Charleston, SC	30.5cm (12in) PSC	OED	Delmag D30-23	40
9	Charleston, SC	HP305x79 (HP12x53)	Hydraulic	Conmaco C65	7
10	Charlester SC	HP305x79 (HP12x53)	Air	Vulcan 06	6
10	Charleston, SC	30.5cm (12in) PSC	Air	Vulcan 06	18
11	Isle of Palms, SC	20.3cm (8in) Timber	Air	Vulcan 01	16
12	Sullivan's Is., SC	25.4cm (10in) PSC	Air	Vulcan 01	109
13	Kiawah Island, SC	20.3cm (8in) Timber	Air	Vulcan 06	3
14	Kiawah Island, SC	30.5cm (12in) PSC	Air	Vulcan 06	74
15	Charleston, SC	HP305x79 (HP12x53)	Air	Vulcan 06	95
16	Seabrook Is., SC	20.3cm (8in) Timber	Air	Vulcan 01	94
17	Fally Baash SC	30.5cm (12in) PSC	Air	Vulcan 06	4
17	Folly Beach, SC	20.3cm (8in) Timber	Air	Vulcan 06	16
18	Mt. Pleasant, SC	Fordingham 3NA	Vibratory	PVE 1420	46
19	Charleston, SC	30.5cm (12in) PSC	Hydraulic	ICE 115	5
20	Sullivan's Is., SC	25.4cm (10in) Timber	Drop	Drop Hammer	18
21	Charleston, SC	30.5cm (12in) PSC	Hydraulic	ICE 115	6
21	Charleston, SC	30.5cm (12in) PSC	Hydraulic	ICE 75	143
22	Folly Beach, SC	30.5cm (12in) Timber	Drop	Drop Hammer	48
23	Sullivan's Is., SC	20.3cm (8in) Timber	Drop	Drop Hammer	38
				TOTAL	1793



<b>Pioneers in CPT and Pile Datab</b>	یشگامان ارائه و توسعه بانکهای اطلاعاتی				
			<b>CPT و شمعها</b>		
Nottingham (1975)	Florida	, USA			
Meyerhof (1976, 1983)	Canada	a and USA			
Schmertmann (1978)	FHWA	Guidelines			
de Ruiter & Beringen (1979)	North S	Sea, Europe			
Bustamante & Gianesselli (1982)	LCPC,	French Method			
Tummay & Fakhroo (1982)	Louisia	ina, USA			



## 4. Overview of Some CPT & Pile Databases

## Briaud and Tucker (1988) Database

□ Evaluating Performance of 13 methods for determining the bearing capacity and settlement of piles based on the results of SPT, CPT, PMT and dynamic formulas

98 case studies of steel and concrete piles with square, H, circular cross sections

□ Pile lengths between 3 and 25 m

□ The ultimate loads range from 307 to 2536 kN

### CPT & Pile Databases By: Eslami & Moshfeghi

🗞 driven in sand	+ driven, mixed, tip in sand
* driven in clay	X driven, mixed, tip in olay
O bered in clay	





## Alsamman (1995) Database

- □ 95 case records of axial load testing on bored piles
- **29** sites from 8 countries
- □ 48 loading tests in granular, 16 in cohesive and 31 in mixed soils
- □ The diameter of the piles is between 300 and 2130 mm
- □ The embedment depth of the piles is between 4.6 to 42 m



## Eslami and Fellenius (1997) Database

- □ 102 case studies from 40 sites and 13 countries
- □ Clay, silt and sand deposits
- □ Mainly square or circular in sections
- □ Steel and concrete materials
- □ Piles bearing capacity: 80 to 8000 kN





## 4. Overview of Some CPT & Pile Databases

# Abu-Farsakh & Titi (2004) Database

□ Performance of 8 CPT-based methods

□ 35 prestressed square concrete piles

□ The embedment length between 9 & 38 m

□ The section size between 356 & 762 mm

29 piles driven in clay and 9 in layered soils

Clay (number of piles) 16	Clay and Sand (number of piles) 2
(number of piles)	(number of piles)
16	2
	<u> </u>
4	—
1	1
2	—
3	6
26	9
10 15 20	25 30 35
	1 2 3

نگرش نوین بر طراحی و اجرای یی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸



## 4. Overview of Some CPT & Pile Databases

### CPT & Pile Databases By: Eslami & Moshfeghi

## UWA (Lehane et al., 2005) Database

□ 77 tensile and compressive loading tests

Driven concrete piles in sand

□ Piles length: 5 to 80 m (mainly 10 to 20 m)

□ The diameters mainly less than 800 mm

□ The bearing capacity mainly less than 5 MN





## ZJU-ICL Database (2015)

- Zhejiang University/Imperial College London (ZJU-ICL) database
- Developed by Yang et al. (2015) Site ID No. 3: K27, Wuhu, China
- □ 115 driven piles in sand

Openly accessible





CPT & Pile Databases By: Eslami & Moshfeghi

## 4. Overview of Some CPT & Pile Databases

# Kempfert & Becker (2010)





### Amirkabir University of Technology Department of Civil and Environmental Engineering

## AUT;GEO-CPT&PILE DATABASE

GEOTECHNICAL INFORMATION, CPT AND CPTU DATA AND PILE LOADING TESTS RECORDS

## **Developed by:**

- Engr. Sara Moshfeghi
- Dr. Abolfazl Eslami
- Dr. S. Majdeddin MirMohammad Hosseini

## Finalized by:

- Dr. Abolfazl Eslami
- Dr. Abbas Soroush
- Engr. Sara Moshfeghi
- Engr. AmirHossein Vojgani



## توزيع جغرافيايي 600 داده بانك اطلاعاتي دانشگاه صنعتي اميركبير

600 Records of pile axial loading tests along with adjacent CPT or CPTu profiles.





**CPT & Pile Databases By: Eslami & Moshfeghi** 

## 5. Introduction to AUT;Geo-CPT&Pile Database

Digitizing load-displacement diagrams derived from loading tests and CPT profiles using the GetData Graph Digitizer 2.2 software.



اطلاعات گرافیکی مندرج در بانک



**CPT & Pile Databases** 

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## **Piles Specifications**





نگرش نوین بر طراحی و اجرای پی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸



## **Database structure-General Records Form**

AUT	-CPT&Pile Data		&PILE DA'	ΓABASE						
	Home	General Record	s CPT Data	Piles	Sour	rces	Search			
	GENE	RAL RECOR								
	Case No.	Case ID	Reference	Location	Shape	Material	Installation	b (mm)	D (m)	
•	1	001-A&M1	Eslami (1996)	Mass., U.S.A.	Square	Concrete	Driven	400	8.8	Details
	2	001-A&M11	Eslami (1996)	Mass., U.S.A.	Square	Concrete	Driven	350	5.5	Details
	3	001-A&M14	Eslami (1996)	Mass., U.S.A.	H Pile	Steel	Driven	256	8.5	Details
	4	001-A&M16	Eslami (1996)	Mass., U.S.A.	H Pile	Steel	Driven	256	9.7	Details
	5	001-A&M19	Eslami (1996)	Mass., U.S.A.	Square	Concrete	Driven	400	8.4	Details
	6	001-A&M20	Eslami (1996)	Mass., U.S.A.	Square	Concrete	Driven	400	21	Details

ساختار بانک اطلاعاتی
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## **Database structure-CPT Data Form**

	JT- CPT&PILE	E DATABA	SE						
Home	General Records CP	T Data Pi	les Sources	Se	arch				
CPT DA	ТА								
Case No	172	CP	T Depth (m)	8					
Case ID	066-ISC2T1	CP	T Digitization Intervals (m)	0.1					
	CPTL	OGS				CPT DI GI	TALS		
q(MP)	i) 5, (NPa)	u (NPa)	n (19	Z (m)	q <sub>c</sub> (MPa)	f <sub>s</sub> (MPa) u	2 (MPa) u <sub>0</sub> (	MPa) R <sub>f</sub> (%)	
0 5		u (NPa)	002 0 5 10	0.10	3.235	f <sub>s</sub> (MPa) u	2 (MPa) u <sub>0</sub> (2 0.000 0.0	000 0.000	
,	i) 5, (NPa)	-0.04 -0.02 0.00 (		0.10 0.20	3.235 4.857	f, (MPa) u 0.000 0.043	2 (MPa) u <sub>0</sub> ( 0.000 0.0 -0.003 0.0	000 0.000 000 0.887	
s.(MP)	i) 5, (NPa)	u (NPa)		0.10 0.20 0.30	3.235 4.857 3.830	f, (MPa) u 0.000 0.043 0.141	2 (MPa) u <sub>0</sub> (2 0.000 0.0 -0.003 0.0 -0.019 0.0	000 0.000 000 0.887 000 3.689	
s_(WP)	i) 5, (NPa)	-0.04 -0.02 0.00 (		0.10 0.20	3.235 4.857	f, (MPa) u 0.000 0.043	2 (MPa) u <sub>0</sub> ( 0.000 0.0 -0.003 0.0 -0.019 0.0 -0.022 0.0	000 0.000 000 0.887	
				0.10 0.20 0.30 0.40	3.235 4.857 3.830 3.003	f, (MPa) u 0000 0043 0141 0183	2 (MPa) u <sub>0</sub> ( 0.000 0.0 -0.003 0.0 -0.019 0.0 -0.022 0.0 -0.023 0.0	000 0.000 000 0.887 000 3.689 000 6.094	
				0.10 0.20 0.30 0.40 0.50 0.60 0.70	3.235 4.857 3.830 3.003 2.931 2.175 2.387	f, (MPa)         u           0.000         0.043           0.141         0.183           0.181         0.170           0.134         0.134	2 (MPa)         u <sub>0</sub> (t)           0.000         0.0           -0.003         0.0           -0.019         0.1           -0.022         0.1           -0.023         0.1           -0.025         0.1           -0.005         0.1	000 0.000 000 0.887 000 3.689 000 6.094 000 6.163 000 7.837 000 5.607	
				0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80	3.235 4.857 3.830 3.003 2.931 2.175 2.387 2.633	f, (MPa)         u           0.000         0.043           0.141         1.83           0.181         0.170           0.134         0.128	2 (MPa)         u <sub>0</sub> (t)           0.000         0.0           -0.003         0.0           -0.019         0.0           -0.022         0.0           -0.023         0.0           -0.025         0.0           -0.005         0.0           -0.005         0.0	000         0.000           000         0.887           000         3.689           000         6.094           000         6.163           000         7.837           000         5.607           000         4.857	
				0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90	3.235 4.857 3.830 3.003 2.931 2.175 2.387 2.633 2.633	f, (M Pa)         u           0.000         0.043           0.141         0.183           0.181         0.170           0.134         0.128           0.136         0.136	(MIPa)         ug (2           0.000         0.0           -0.019         0.1           -0.022         0.1           -0.023         0.1           -0.025         0.1           -0.005         0.1           -0.005         0.1           -0.003         0.1	000         0.000           000         0.887           000         3.689           000         6.094           000         6.163           000         5.607           000         4.857           000         5.175	
			5222 0 5 20 - 2	0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00	3.235 4.857 3.830 3.003 2.931 2.175 2.387 2.633 2.633 2.409	f. (MPa)         u           0000         0043           0141         0183           0181         0170           0134         0128           0126         0120	(MPa)         u <sub>0</sub> (0           0.000         0.1           -0.003         0.1           -0.019         0.1           -0.022         0.1           -0.023         0.1           -0.023         0.1           -0.023         0.1           -0.005         0.1           -0.003         0.1           -0.003         0.1           -0.003         0.1           -0.003         0.1	000         0.000           000         0.887           000         3.689           000         6.094           000         7.837           000         5.607           000         4.857           000         4.977	
			5252 0 5 5 20 - 2	0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00 1.10	3.235 4.857 3.830 3.003 2.931 2.175 2.387 2.633 2.633 2.633 2.409 2.797	f, (M Pa)         u           0000         0043           0141         0183           0181         0170           0134         0128           0136         0120           0117         0117	Q (MPa)         up (0           0.000         0.           -0.003         0.           -0.019         0.           -0.023         0.           -0.023         0.           -0.005         0.           -0.002         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.001         0.           -0.002         0.	000         0.000           000         0.887           000         3.689           000         6.094           000         7.837           000         5.607           000         4.857           000         5.175           000         4.185	
				0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00 1.10 1.20	3.235 4.857 3.830 3.003 2.991 2.175 2.387 2.633 2.633 2.633 2.409 2.797 2.551	f, (M Pa)         u           0000         043           0141         0183           0181         0170           0134         0128           0135         0136           0130         0117	2 (MPa)         up (2           0.000         0.           -0.003         0.           -0.019         0.           -0.022         0.           -0.023         0.           -0.005         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.002         0.	000         0.000           000         0.887           000         3.689           000         6.163           000         5.607           000         4.857           000         5.175           000         4.185           000         4.185           000         5.112	
				0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00 1.10	3.235 4.857 3.830 3.003 2.931 2.175 2.387 2.633 2.633 2.633 2.409 2.797	f, (M Pa)         u           0000         0043           0141         0183           0181         0170           0134         0128           0136         0120           0117         0117	Q. (MPa)         up (P.           0.000         0.           -0.003         0.           -0.019         0.           -0.022         0.           -0.023         0.           -0.023         0.           -0.023         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.002         0.           -0.002         0.           -0.002         0.           0.000         0.	000         0.000           000         0.887           000         3.689           000         6.094           000         7.837           000         5.607           000         4.857           000         5.175           000         4.185	
				0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00 1.10 1.20 1.30	3.235 4.857 3.830 3.003 2.931 2.175 2.387 2.633 2.633 2.633 2.409 2.797 2.551 2.760	f, (MPa)         u           0000         0/43           0141         0.183           0181         0.170           0134         0.128           0136         0.120           0136         0.120           0137         0.133	Q (MPa)         up (P.           0.000         0.           -0.003         0.           -0.019         0.           -0.022         0.           -0.005         0.           -0.002         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.002         0.           -0.002         0.           -0.002         0.           -0.002         0.	000         0.000           000         0.887           000         3.689           000         6.094           000         6.163           000         5.607           000         5.175           000         4.1857           000         4.1877           000         4.185           000         5.112           000         4.801	
				0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00 1.10 1.20 1.30 1.40 1.50 1.60	3.235 4.857 3.830 3.003 2.931 2.175 2.387 2.633 2.633 2.633 2.409 2.797 2.551 2.760 2.703	f, (MPa)         u           0000         0043           0141         0183           0181         0170           0134         0136           0136         0120           0117         0130           0133         0142	Q (MPa)         up (P.           0.000         0.           -0.003         0.           -0.019         0.           -0.023         0.           -0.023         0.           -0.005         0.           -0.002         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.001         0.           -0.002         0.           -0.002         0.           -0.002         0.           -0.002         0.           -0.002         0.           -0.002         0.           -0.002         0.	000         0.000           000         0.887           000         3.689           000         6.163           000         5.607           000         5.175           000         4.185           000         4.185           000         4.185           000         4.185           000         4.211           000         4.201           000         5.209           000         5.528	
				0.10 0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00 1.10 1.20 1.30 1.40 1.50	3.235 4.857 3.830 3.003 2.931 2.175 2.887 2.633 2.409 2.797 2.551 2.760 2.703 2.588	f, (MPa)         u           0000         0043           0141         0183           0181         0170           0134         0126           0120         0117           0130         0141           0133         0142	Q.(MPa)         up (P.           0.000         0.           -0.003         0.           -0.003         0.           -0.019         0.           -0.022         0.           -0.005         0.           -0.005         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.002         0.           -0.003         0.           -0.002         0.           -0.002         0.           -0.003         0.           -0.002         0.           -0.003         0.           -0.002         0.           -0.002         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.003         0.           -0.010         0.	000         0.000           000         0.887           000         3.689           000         6.094           000         7.837           000         5.607           000         4.857           000         4.185           000         4.185           000         4.211           000         4.221           000         4.211           000         5.246           000         5.209	

ساختار بانک اطلاعاتی-دادههای CPT



## **Database structure-**Piles Information

I AUT-CPT&Pile Database	AUT- CPT&PILE DATABASE
AUT- CPT&PILE DATABASE Home General Records CPT Data Piles Sources Search Bored Drilled Displacement Driven Concrete H Helical Pipe Other Types	Home     General Records     CPT Data     Piles     Sources     Search       Bored     Drilled Displacement     Driven Concrete     H     Helical     Pipe     Other Types       BORED PILES     Case No     13     Case ID     001-A&M32
BORED PILES         Load Test(s) Information         Test No.5       Test No.6       Test No.7       Test No.9         Test No.1       Test No.2       Test No.3       Test No.4         Type of Test and Loading       Static Compression, SML       Image: Static Compression, SML       Image: Static Compression, SML         Time Interval Between       Installation and Loading, Days       Image: Static Compression, SML       Image: Static Compression, SML         Toe Capacity, Rt , kN       Image: Static Compression, SML       Image: Static Compression, SML       Image: Static Compression, SML         Shaft Capacity, Rs, kN       Image: Static Compression, SML       Image: Static Compression, SML       Image: Static Compression, SML	Pile Characteristics   Shape   Round   Material   Concrete   Installation   Bored   Embedment Length, D (m)   10.6   Diameter, b (mm)   350   Cross Sectional Area, At (m2)   0.0962   Perimeter (m)   1.100
Total Capacity, Ru, kN     1160       Remarks     0       Record: H < 1 of 55     H HC       K No Filter     Search	Record: H 1 of 55 + H R No Filter Search

ALIT-CPT&Pile Datab

نگرش نوین بر طراحی و اجرای پی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸



CPT & Pile Databases By: Eslami & Moshfeghi

## 5. Introduction to AUT;Geo-CPT&Pile Database

## **Database structure- Sources**

🖃 AUT-CPT&Pile Database	
AUT- CPT&PILE DATABASE	ساختار بانک اطلاعاتی-منابع
Home General Records CPT Data Piles Sources Search	
SOURCES	
Source No 003 Reference Seo et al. (2009)	
Assessment of the Axial Load Response of an H Pile Driven in Multilayered Soil Hoyoung Seo <sup>1</sup> ; Irem Zeynep Yilditm <sup>2</sup> ; and Monica Prezzi <sup>3</sup>	
clean said These methods are sometimes used for H piles as well, aven fough the arist lead response of H piles is different from that of pipe piles. Furthermore, in reality, soil profiles often consist of matiple) layers of site lists in a mixed soil is very that the user of the sizes. Therefore, accurate prediction of the ultimate bearing capacity of H piles drives in a mixed soil is very challenging. In addition, although results of well documented load tests on pipe piles are available, the listerature contains limited information on the design of II piles. Most of the current design methods for driven piles becyclic recommendations for II piles. In order to evaluate the static load response of an II pile, fully instrumented axial load tests or dray, sit and state. The base of the H pile verse evaluates the static load response of an II pile, fully instrumented axial load tests or dray, sit and state. The base of the H pile verse evaluate the static load response of an II pile, fully instrumented axial host tests of the relation of the current design performed to characterize the static soft response of an II pile and of the pile icad tests. It also compares the measured pile resistances with those predicted with no ill property- and in situ tast-based methods.	
Record: I4 < 3 of 46     H     K     Search	



## **Database structure-Search & Search Results**

Resi	ılts								SEARCH
Case No	Case ID	Reference	Location	Shape	Material	Installation	b (mm)	<b>F</b>	Search by I
68	001-L&D31	Eslami (1996)	III., U.S.A.	Pipe	Steel	Driven	300		Installation
72	001-L&D32	Eslami (1996)	III., U.S.A.	Pipe	Steel	Driven	300		Shape
73	001-L&D34	Eslami (1996)	III., U.S.A.	Pipe	Steel	Driven	350		<u>Search by S</u> CPT data
74	001-L&D35	Eslami (1996)	III., U.S.A.	Pipe	Steel	Driven	350		Soil Typ
75	001-L&D37	Eslami (1996)	III., U.S.A.	Pipe	Steel	Driven	400		
76	001-L&D38	Eslami (1996)	III., U.S.A.	Pipe	Steel	Driven	400		
101	001-N&SBI42	Eslami (1996)	Fla., U.S.A.	Pipe	Steel	Driven	273	Rec	ord: H ⊣ 1 of 1
242	176-DUNKIRK C1C	Jardine & Standing (2000)	France	Pipe	Steel	Driven	457	10.02	Details
243	176-DUNKIRK C1T	Jardine & Standing (2000)	France	Pipe	Steel	Driven	457	10.02	Details
244	176-DUNKIRK JP1	Jardine & Standing (2000)	France	Pipe	Steel	Driven	457	10.00	Details

AUT-CPT&Pile Database	CPT&PILE D	ATABASE
Home Gener	ral Records CPT Data	Piles Sources Search
SEARCH		Search
Search by Pile C	haracteristics:	
Installation Shape		Diameter Range (mm)     -       Embedment Length Range (m)     -
Search by Soil T	ype and CPT data:	Search by Loading Test Data:
<u>CPT data</u>	fs 🔲 u 🔳	Type of Test and Loading
Soil Type:	Sand 🔲 Clay 🔲	Seperated Shaft and Toe Resistance 🔳
	Mix 🔲	
Record: M < 1 of 1 > >	▶¤ 🕅 🕅 No Filter Search	
0.02 Details		
0.02 Details		ساختار بانک اطلاعاتی- جستجو
0.00 Details		<b>J</b>

نگرش نوین بر طراحی و اجرای پی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸







نگرش نوین بر طراحی و اجرای پی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸

## 5. Introduction to AUT;Geo-CPT&Pile Database









## 6. Typical Implementations

### Moshfeghi & Eslami (2015-2019)



International Journal of Geotechnical Engineering

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Taylor & Francis

# Study on pile ultimate capacity criteria and CPT-based direct methods

### Sara Moshfeghi and Abolfazl Eslami\*

Due to the variety of current Cone Penetration Test (CPT)-based methods of estimating the pile bearing capacity, for optimum design, it is necessary to evaluate the performance of such methods in various geotechnical conditions. Geotechnical databases including piling and *in situ* testing records have been recognised as useful tools for analysis, design and economical construction. In order to evaluate current CPT-based pile bearing capacity methods, AUT-CPT and Pile database has been compiled including 450 full scale pile load tests and CPT sounding records. This database consists of different pile types with a relatively wide range of geometries and various soil conditions. Forty-three records of piles driven in sand deposits were then employed to evaluate effects of ultimate capacity interpretation criteria from load displacement diagrams. The Brinch Hansen 80% criterion and the load at the displacement of 10% of the pile diameter were compared to estimated capacities from 10 CPT-based design methods currently used in practice. The Brinch Hansen 80% criterion and the load at the displacement of 10% of the pile diameter lead to reasonable results, the Brinch Hansen 80% criterion showed less scatter. For evaluating the accuracy and the precision of CPT-based methods, the results were compared to estimated capacities. Methods with the best performance are introduced. Generally, comparisons indicate that the CPT-based methods mainly predict the pile capacity with reasonable accuracy.

شامل ۴۳ مورد عملی شمع و CPT
 انطباق پذیری روشهای تفسیر نمودار بارگذاری شمع
 ارزیابی ظرفیت باربری کششی و فشاری شمع

نگرش نوین بر طراحی و اجرای پی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸

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## 6. Typical Implementations

**CPT & Pile Databases By: Eslami & Moshfeghi** 



Displacement (mm)

بررسی روش های تفسیر نمودار بارگـذاری شمع ها و انطبـاق پـذیری نتـایج آنهـا بـا روشهای مبتنی بر CPT



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CPT & Pile Databases By: Eslami & Moshfeghi

### Moshfeghi & Eslami (2015-2019)







GEORISK https://doi.org/10.1080/17499518.2018.1478105



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# Failure analysis of CPT-based direct methods for axial capacity of driven piles in sand

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#### ABSTRACT

Due to variety of current pile bearing capacity methods based on cone penetration test (CPT) measurements, there is always a need for evaluating performance of existing methods to make proper choices of methods as well as safety factors for optimum design. In this regard, geotechnical databases are known as useful tools which facilitate evaluation of existing methods. This paper deals with axial bearing capacity of driven piles in sand using CPT-based methods. A database of seventy-six records is employed to analyze different criteria of interpreting static pile load test results to select the most consistent approach with the CPT-based methods. Then, performance of nine commonly used direct CPT-based methods was evaluated. Finally, via a failure probability and cost optimisation approach, optimum safety factors are presented and discussed. Analysis of different failure criteria shows that the Hansen 80% criterion leads to more consistent results with the CPT-based methods. In addition, almost all of the investigated methods showed promising performance. The attained safety factors range from 1.6 to 3.1 for all records, 1.4 to 3.1 for piles in compression, and 1.4 to 2.2 for the piles in tension. Then, efficiency of methods was evaluated and the methods with higher efficiency are introduced.

ARTICLE HISTORY

Received 1 July 2016 Accepted 13 April 2018

KEYWORDS Database; CPT; pile bearing capacity; load test; failure interpretation criterion; optimum safety factor; probability of failure



مبتنی بر CPT:

🗆 ۷۶ مورد عملی شمع های کوبشی در ماسه

🗆 تحلیل گسیختگی

### 🗖 تعیین ضرایب اطمینان بهینه و کارایی روشها



تعیین ضرایب اطمینان بهینه و کارایی روش هـای مبتنی بر CPT







7.0







Factor of Safety







CPT & Pile Databases By: Eslami & Moshfeghi

Min. S.F.

for Risk=0

2.4

2.3

1.5

2

2.5

2.2

3

2.4

3.1

2.2

### Moshfeghi & Eslami (2015-2019)

کارایی روش هـای	ی <mark>نان بهینه و</mark>	تعيين ضرايب اطه
		مبتنی بر CPT

Method	FS <sub>opt</sub> Method		Safety Factor					
Meyerhof-1976	2.4		1.5	2	2.5	3	3.5	
Schmertman-1978	1.5-2.3	Meyerhof-1976	15.9	5.7	0	0	0	
		Schmertman-	5.7	2.3	0	0	0	
Dutch-1979	1.4, 1.5	1978	5.7	2.5	0	0	0	
LCPC-1982	2.0	Dutch-1979	0	0	0	0	0	
Unicone-1997	1.6-2.5	LCPC-1982	15.9	0	0	0	0	
UWA-2005	1.7, 2.2	Unicone-1997	17.0	2.3	0	0	0	
NGI-2005	1.8,2.5	UWA-2005	7.9	1.1	0	0	0	
Fugro-2005	2.4	NGI-2005	15.7	7.9	1.1	0	0	
ICP-2005	1.6-3.1	Fugro-2005	14.6	4.5	0	0	0	
German-2010	2.2	ICP-2005	12.4	4.5	3.4	1.1	0	
		German-2010	16.8	4.5	0	0	0	

نگرش نوین بر طراحی و اجرای پی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸



### Moshfeghi & Eslami (2015-2019)

MARINE GEORESOURCES & GEOTECHNOLOGY https://doi.org/10.1080/1064119X.2018.1448493 Taylor & Francis Taylor & Francis Group

#### Check for updates

# Reliability-based assessment of drilled displacement piles bearing capacity using CPT records

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Department of Civil and Environmental Engineering, Amirkabir University of Technology, AUT, (Tehran Polytechnic), Tehran, Iran

#### ABSTRACT

Drilled displacement piles (DDPs) are known as an alternative to conventional foundations in coastal areas, given the elimination of environmental impacts and difficulties caused by installation process of driven piles and more consistency with environment. Despite increasing employment of these piles, the extent of research works does not yet suffice the requisites to reach a routine design. This paper aims to analyze six cone penetration test (CPT)-based methods of determining the bearing capacity of DDP. The statistical and reliability-based approaches were used in two parts of assessing performance of the methods with respect to soil-pile characteristics followed by evaluating reliability of the prediction outcome. A database is compiled including 65 DDP load tests with adjacent CPT profiles. Performance of the methods are analyzed. Finally, a reliability parameter, i.e., confidence interval, is introduced to demonstrate a more realistic insight into the evaluations by expressing performance of the methods in terms of a range for possible average values of the predictions ratios, rather than simply an arithmetic mean. The study reveals that the commonly used CPT-based methods which have not been specifically developed for DDP show great potential for design. The results indicate that the investigated methods can have promising performance if some modifications are applied.

#### **ARTICLE HISTORY**

Received 10 November 2017 Accepted 1 March 2018

#### KEYWORDS

Bearing capacity; confidence interval; CPT methods; drilled displacement pile (DDP); reliability-based evaluation





**CPT & Pile Databases By: Eslami & Moshfeghi** 

#### Moshfeghi & Eslami (2015-2019)





Evaluation results of CPT-based methods based on shaft shapes



### Moshfeghi & Eslami (2015-2019)





**German Method** 





**CPT & Pile Databases** By: Eslami & Moshfeghi



400

Depth

Abstract The true distribution of both pile shaft and toe resistances along depth, has been an important issue in geotechnical engineering. Twenty four pile load test case records of deep foundation projects, where CPT, Cone Penetration Test, soundings were also advanced close to piles locations, throughout the world have been compiled for investigations and analyses. The geomaterial at these sites are homogenous, including sandy, clayey and silty soils. Four different methods for determining pile bearing capacity comprising the method based on critical depth concept, recommended approaches by CFEM, Canadian Foundation Engineering Manual 2006 (Unified

method), American Petroleum Institute (API), and CPT-based methods are presented, compared and discussed. In addition, the influence of factors such as soil friction angle variations, calculated from q<sub>c</sub>, cone tip resistance, and overburden stress, are taken into account to perform indirect calculations. Direct and indirect CPT-based calculations on the pile capacity are studied to investigate the actual pile toe and shaft resistances distribution along depth. The comparisons reveal that in practice and in observations from full scale tests, shaft and toe resistances follow a nonlinear and gradual trend beyond the certain depth. However, it is not in agreement with conventional linearconstant or relatively linear distribution concept and some recommended codes.





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## 6. Typical Implementations

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**توزیع مقاومت کف و جدار شمع در عمق مبتنی بر نتایج CPT-**بررسي تئوري عمق بحراني

Comparison of the results reveals that bearing capacity at the critical depth, **is neither linear-constant, nor linear** as

suggested by Unified codes.

Rather, the calculations in direct methods including CPT-

based and UniCone show that bearing capacity gradually

varies with depth and have a gradual decreasing trend.

Total pile resistance distribution versus normalized pile geometry (L/d) for cases No. 3, 7, 10, 12



**CPT & Pile Databases By: Eslami & Moshfeghi** 

### Valikhah & Eslami (2017-2019)

International Journal of Civil Engineering https://doi.org/10.1007/s40999-018-0388-7

**RESEARCH PAPER** 

#### Load–Displacement Behavior of Driven Piles in Sand Using CPT-Based Stress and Strain Fields

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Received: 24 September 2018 / Revised: 24 November 2018 / Accepted: 10 December 2018 © The Author(s) 2018

#### Abstract

The bearing capacity of piles is often estimated by a variety of methods such as the limit equilibrium or the limit analysis. In contrast, the load–displacement behavior, which should not be disregarded in common practices, cannot be obtained as simply as the bearing capacity. The reason is its dependency on the stress and the strain (or the displacement) fields around the pile. In the current work, attempt has been made to predict the load–displacement behavior of driven piles in sand by direct and indirect implementation of the cone penetration test (CPT) data into the displacement field. CPT often serves as a very successful in situ test which provides a close link between the soil resistance and the bearing capacity, although it brings no direct information. A rather simple procedure is presented to indirectly use the CPT data to find the stress and strain fields. While the pattern of the failure mechanism has been obtained by the method of stress characteristics, the displacement (and strain) field has been found by the kinematics of the failure mechanism. The proposed procedure has been calibrated and verified by 98 case histories including pile load test results in conjunction with CPT data. Comparisons made by this new method show that the CPT-based method of stress characteristics can be successfully used in load–displacement prediction of driven piles.

Keywords Pile · CPT · Load-displacement · Stress characteristics method · Displacement field



CrossMark







**CPT & Pile Databases By: Eslami & Moshfeghi** 

### Valikhah & Eslami (2017-2019)



نگرش نوین بر طراحی و اجرای پی های عمیق (شمع ها) – ۱ آبان ۱۳۹۸



### Valikhah & Eslami (2017-2019)

Arabian Journal for Science and Engineering https://doi.org/10.1007/s13369-019-04034-y

**RESEARCH ARTICLE - CIVIL ENGINEERING** 

#### CPT-Based Nonlinear Stress–Strain Approach for Evaluating Foundation Settlement: Analytical and Numerical Analysis

Fatemeh Valikhah<sup>1</sup> · Abolfazl Eslami<sup>1</sup>

Received: 9 May 2019 / Accepted: 16 July 2019 © King Fahd University of Petroleum & Minerals 2019

#### Abstract

Due to complexities in soil-foundation interaction and nonlinear behavior of subsoil, considerable uncertainty is involved in the foundation settlement evaluation. In the present paper, a new analytical approach is proposed to estimate the foundation settlement based on soil behavior classification charts developed from CPT records. The approach is founded on the Janbu nonlinear stress-strain method. However, instead of using fixed parameters in the Janbu method, the variable coefficients are used depending on geomaterial properties. Also, in the proposed approach, the scale effect is taken into account for foundation width considering soil stiffness. The proposed procedure is calibrated and verified by a data bank containing 46 case histories including 22 square, 17 circular and 7 rectangular foundations with widths varying between 0.3 and 2.4 m in conjunction with CPT data. Furthermore, the numerical finite difference analysis using a CPT-based stress characteristics method is carried out to validate the proposed approach for the prediction of foundation settlement. The accuracy of the calculations done by the proposed and some available common methods is investigated. Comparisons based on statistical and probabilistic methods apparently reveal that the proposed approach calculates the foundation settlement promisingly.

Keywords Nonlinear stress-strain · Settlement · CPT data · Stiffness modulus · Analytical and numerical analysis · Data bank

**CPT & Pile Databases By: Eslami & Moshfeghi** 

روش مبتنی بر نتایج CPT برای تخمین نشست پیها **(حج) مورد یی سطحی)** 

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### Valikhah & Eslami (2017-2019)

Janbu (1967) Method for Foundation Settlement Estimation:

وش مبتنی بر نتایج CPT برای تخمین نشست پیها  

$$\varepsilon = \frac{\Delta H}{H} \quad \varepsilon = \frac{1}{mj} \left[ \left( \frac{\sigma'_0 + \Delta \sigma'}{100} \right)^j - \left( \frac{\sigma'_0}{100} \right)^j \right]$$

Range of modulus number (m) and stress exponent (j) for different soils in Janbu approach

Malekdoost and Eslami (2011):

$$j = \frac{q_{\rm c} \left[1 + \left(0.05 \log q_{\rm c}\right) \times R_{\rm f}^2\right]}{5^{\log q_{\rm c}} \left(11 \sqrt{R_{\rm f}} + R_{\rm f}^2\right)}$$

 $m = \alpha q_{\rm c}$ 

 $\alpha = 2$ 

Soil type		Modulus number	Stress exponent (j)
Till, very dense to dense		300-1000	1
Gravel		40-400	1
Sand	Dense	250-400	0.5
	Compact	150-250	0.5
	Loose	100-150	0.5
Silt	Dense	80-200	0.5
	Compact	60-80	0.5
	Loose	40-60	0.5
Silty clay and clayey silt	Hard, stiff	20-60	0
	Stiff, firm	10-20	0
	Soft	5-10	0
Soft marine clays and organic clays		5-20	0
Peat		1-5	0



Valikhah & Eslami (2017-2019)

$$\varepsilon = \frac{\Delta H}{H}$$
  $\varepsilon = \frac{1}{mj} \left[ \left( \frac{\sigma'_0 + \Delta \sigma'}{100} \right)^j - \left( \frac{\sigma'_0}{100} \right)^j \right]$ 



**CPT & Pile Databases By: Eslami & Moshfeghi** 

روش مبتنی بر نتایج CPT برای تخمین نشست ییها



Eslami, Lotfi, Infante, Moshfeghi & Eslami (2019)

 $\gamma_{Pile} = 0.0255 \ (V_{Pile})^{0.61} . \ (D_{Pile})^{0.5}$ 

تعیین ظرفیت باربری جداری شمع ها با اسـتفاده از نتایج CPT با لحاظ آثار ابعادی (f<sub>s</sub>-r<sub>s</sub>)

 $r_{s(z)} = k_z \cdot k \cdot f_{s(z)}$ 







R<sub>S</sub> (kN)





GEORISK https://doi.org/10.1080/17499518.2019.1628281



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# Reliability based assessment of axial pile bearing capacity: static analysis, SPT and CPT-based methods

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#### ABSTRACT

Since piles are one of the major geotechnical foundation systems, estimation of their axial bearing capacity is of great importance. Employing different design methods, resulting in a wide range of bearing capacity estimations, complicates the selection of an appropriate design scheme and confirms the existence of model error along with the inherent soil variability in bearing capacity prediction. This paper tends to evaluate different predictive methods in Reliability-Based Design (RBD) framework. In this regard, different static analyses, SPT and CPT-based methods are considered to evaluate which approaches collectively and which method individually, have more reliable predictions for compiled data bank. In order to assess reliability indices and resistance factors, two approaches have been considered, i.e. First Order Second Moment method (FOSM) and First Order Reliability Method (FORM). To investigate the reliability indices for different methods in both RBD approaches, various safety factors and loading ratios have been considered. Also, the Load and Resistance Factor Design (LRFD) resistance factors are calibrated for different target reliability indices and loading ratios. Results show that CPT-based methods are more reliable among other methods. Furthermore, the estimated efficiency ratio, i.e. the ratio of resistance factor to resistance bias factor, confirms this agreement.

#### ARTICLE HISTORY

Received 11 November 2018 Accepted 2 June 2019

#### KEYWORDS

Axial pile bearing capacity; CPT; LRFD; pile foundation; reliability based design

ارزيسابي احتمسالاتي عسدم
قطعیت مدل برای روشهسای
تعیین ظرفیت باربری شمعها



**CPT & Pile Databases** By: Eslami & Moshfeghi



نگرش نوین بر طراحی و اجرای یی های عمیق (شمع ها) - ۱ آبان ۱۳۹۸

ارزيابي احتمالاتي عدم قطعيت مدل براي روشهاي

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#### CPT & Pile Databases By: Eslami & Moshfeghi

## 6. Typical Implementations









## 7. Concluding Remarks

## 1. CPT and Pile (Past):

- Provides continuous records with depth
- Cone penetrometer is considered as a model pile
- Direct and indirect approaches for bearing capacity
- Bearing capacity methods: more than 28 currently used





## 7. Concluding Remarks







CPT & Pile Databases By: Eslami & Moshfeghi









CPT & Pile Databases By: Eslami & Moshfeghi

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